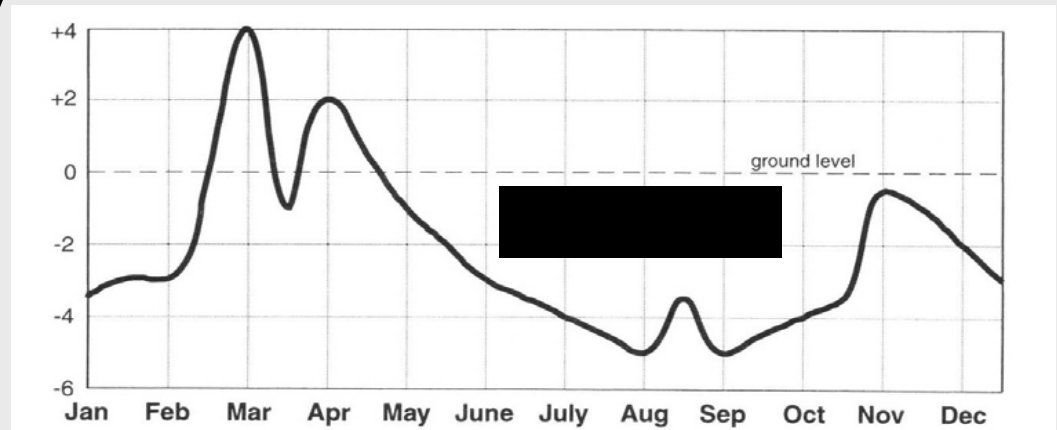


Water budget for wetlands

A wetland's hydroperiod is determined by:

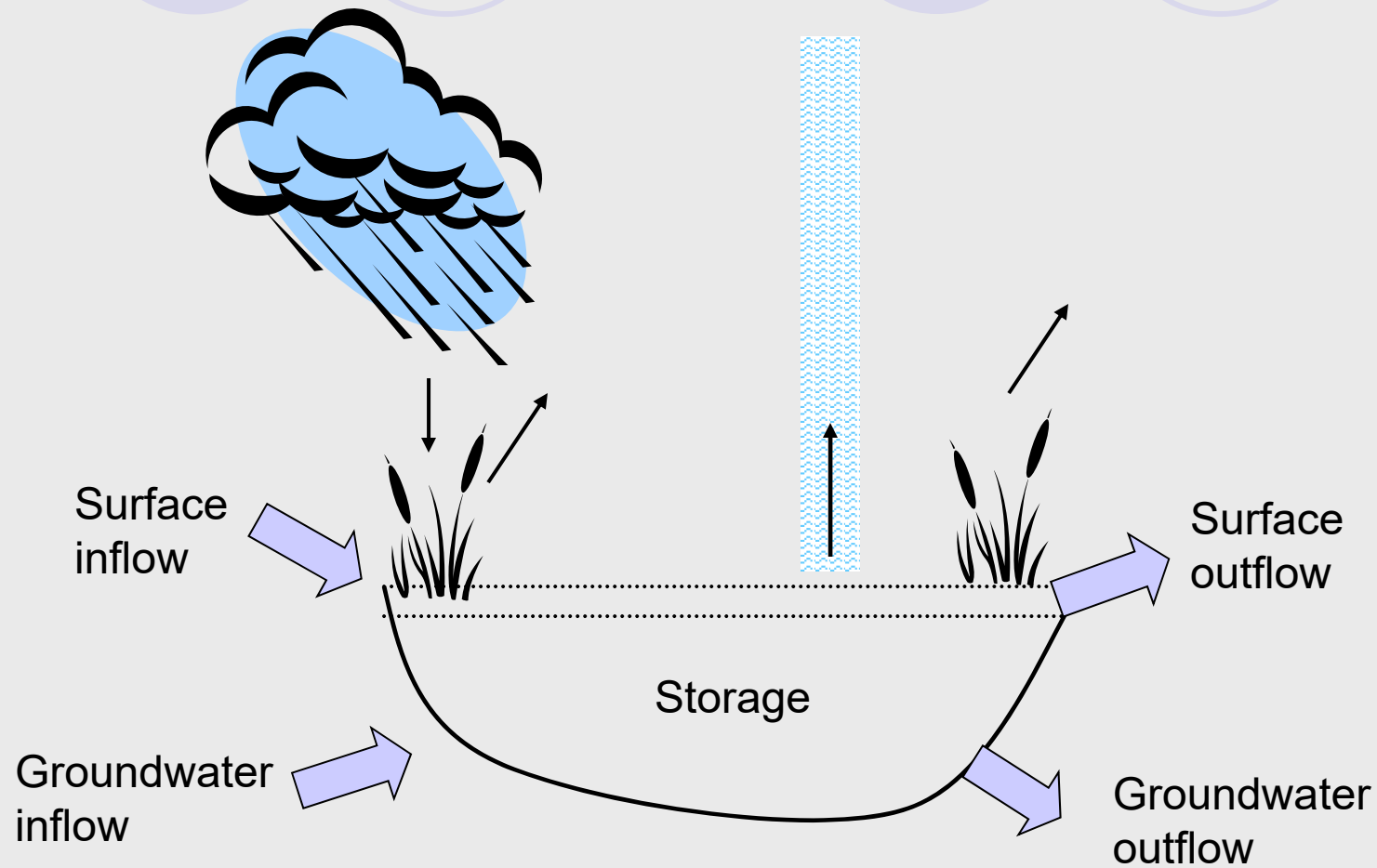
- Inflows – outflows
- Landscape pattern
- Subsurface geology



Water budget: inputs & outputs

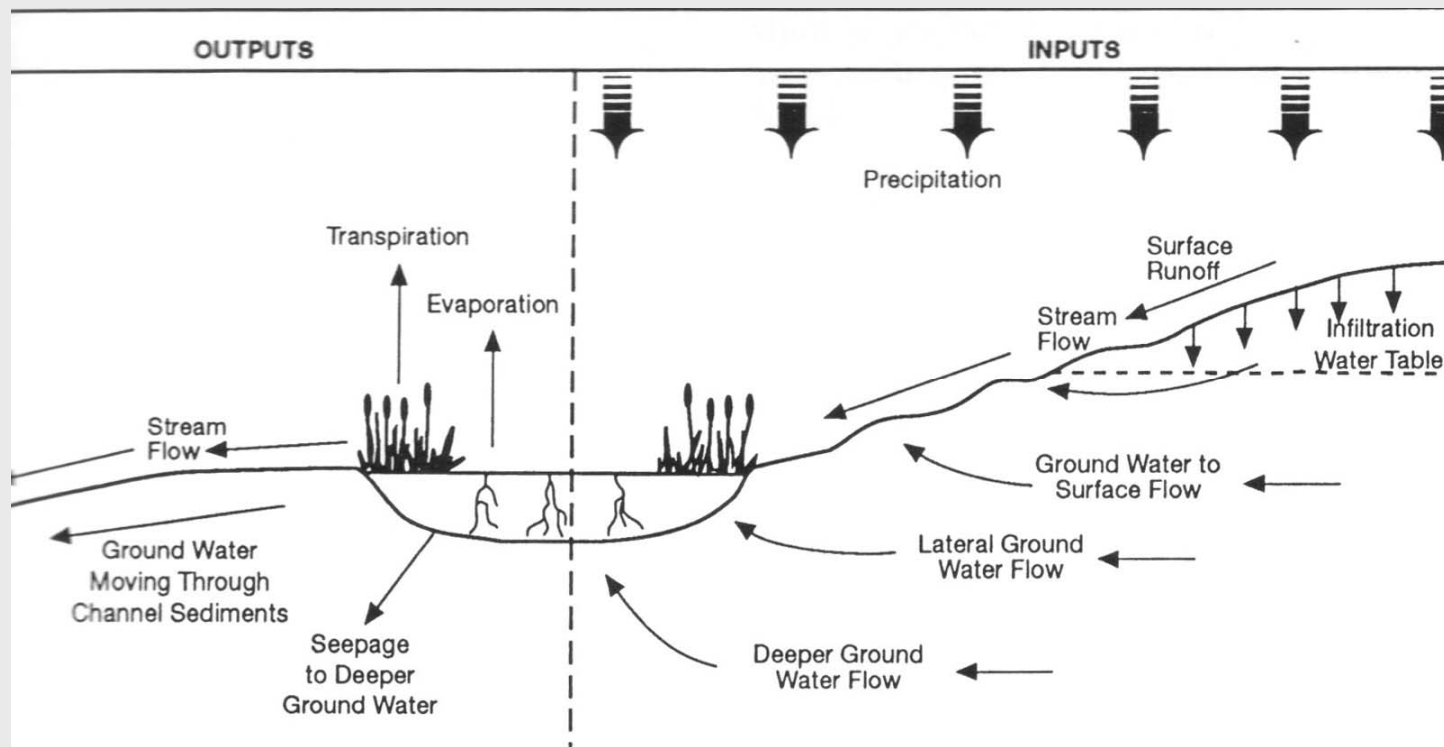


Water budget



Generalized Wetland Water Budget

$$\Delta V/\Delta t = P_n + S_i + G_i - ET - S_o - G_o \pm T$$



Stone and Stone 1994

Water budget for wetlands

$$\Delta V/\Delta t = P_n + S_i + G_i - ET - S_o - G_o \pm T$$

V = Water storage volume

$\Delta V/\Delta t$ = Change in volume per unit time

P_n = Net precipitation

S_i = Surface & stream inflows

G_i = Groundwater inflows

ET = Evapotranspiration

S_o = Surface outflows

G_o = Groundwater outflows

T = Tidal inflow or outflow

UNITS!

$$d = V/A$$

Renewal rate and residence time

$$t^{-1} = Q_t/V \quad V = \text{volume}; Q_t = \text{inflow rate (vol/time)}$$

Renewal rate = rate of water replacement

Residence time = avg time water remains in the basin

Lake	Residence time (t) (years)	Renewal rate (t^{-1}) (per year)
Superior	191	0.005
Michigan	99	
Huron	22	
Erie	2.6	
Ontario	6	


$$\Delta V / \Delta t = P_n + S_i + G_i - ET - S_o - G_o \pm T$$

Precipitation

$$P_g = I + TF + SF$$

I = Interception

TF = Throughfall

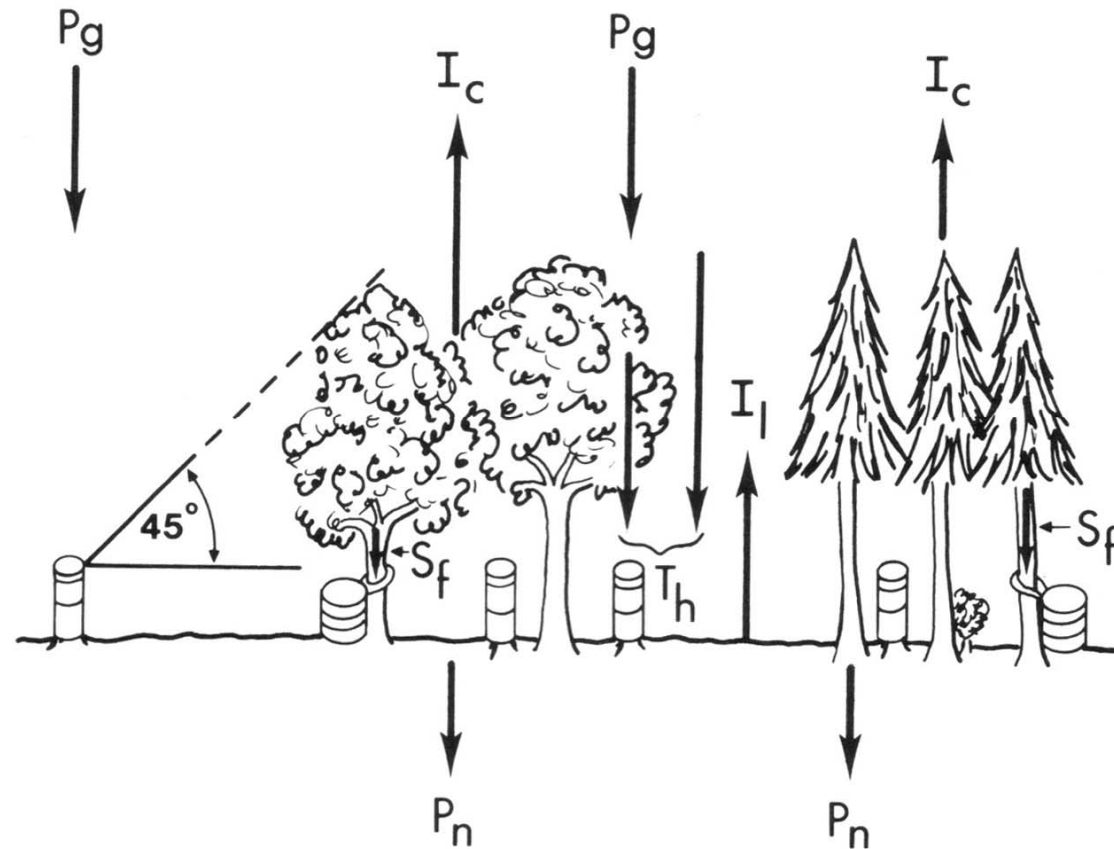
SF = Stemflow

$$P_n = TF + SF$$

or

$$P_n = P_g - I$$

Precipitation



Interception total = $I = I_c + I_l$

The amount reaching the forest floor = $T_h + S_f$

Interception by canopy (overstory + understory) $I_c = P_g - T_h - S_f$

Net precipitation $P_n = T_h + S_f - I_l$

Brooks et al. 1991

2.10. Components of interception (from Hewlett 1982, © Univ. Georgia Press, by permission). I_c = canopy interception; I_l = litter interception; P_g = gross precipitation; P_n = net precipitation; S_f = stemflow; T_h = throughfall.

Does interception really matter?

Forest type	Precip (mm)	Interception (%)	Interception (mm)
Rainforest	281	9	25
Mature white pine	203	9	18
Sitka spruce	100	49	49
Hardwoods	130	13	17
Mixed pines	60	36	22

From Jackson 2006

$$\Delta V/\Delta t = P_n + S_i + G_i - ET - S_o - G_o \pm T$$

Surface flow

Overland flow

$$S_{i(ov)} = R_p P A_w$$

R_p = hydrologic response coefficient

(look up in table; typically < 20%)

P = mean precipitation (m)

A_w = watershed area (m²)

$$S_{i(pk)} = 0.278 C I A_w$$

C = rational runoff coefficient

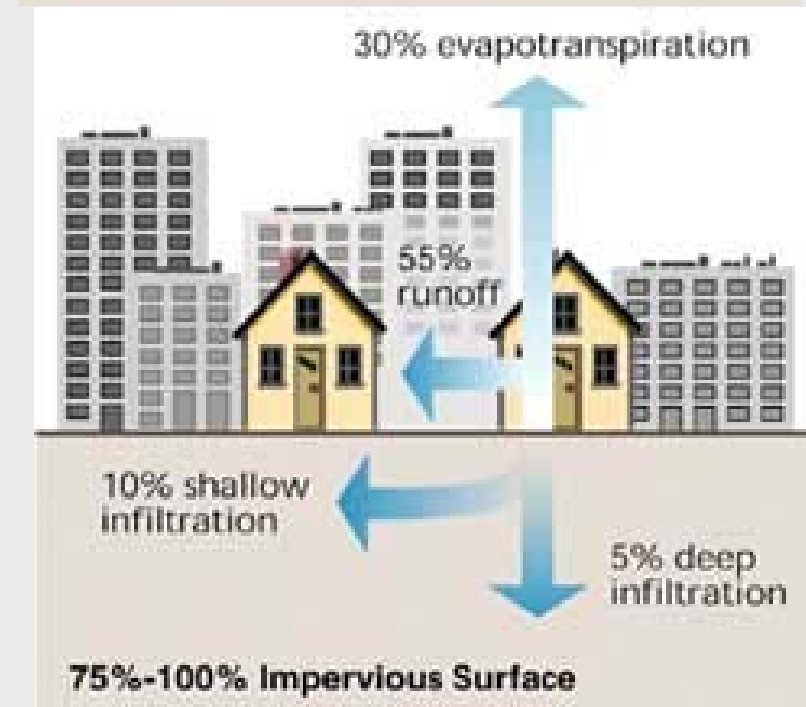
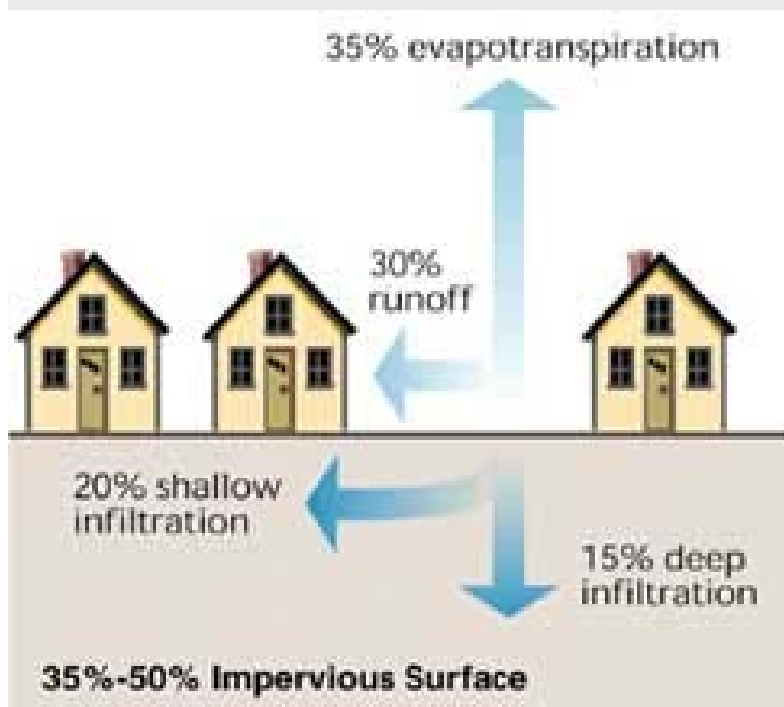
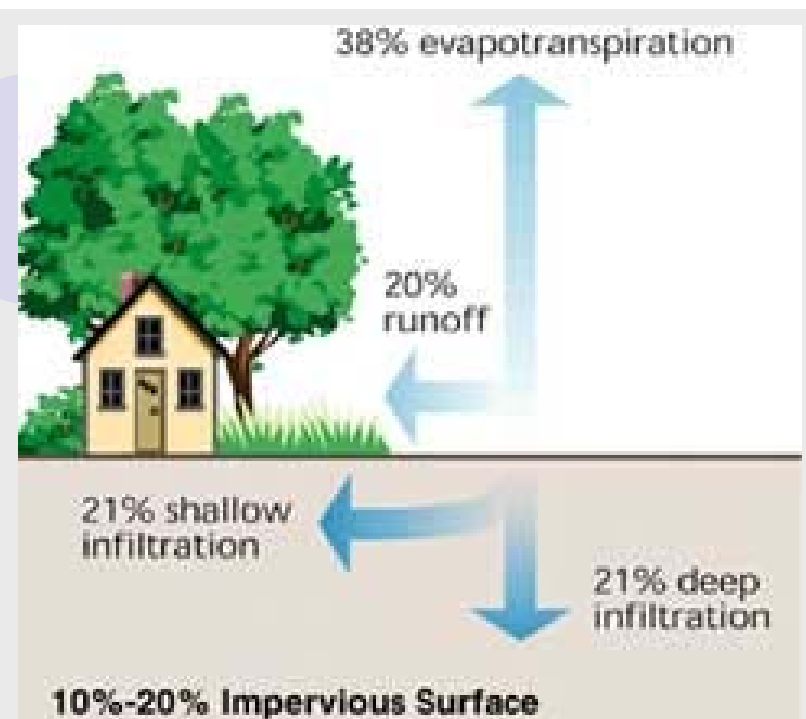
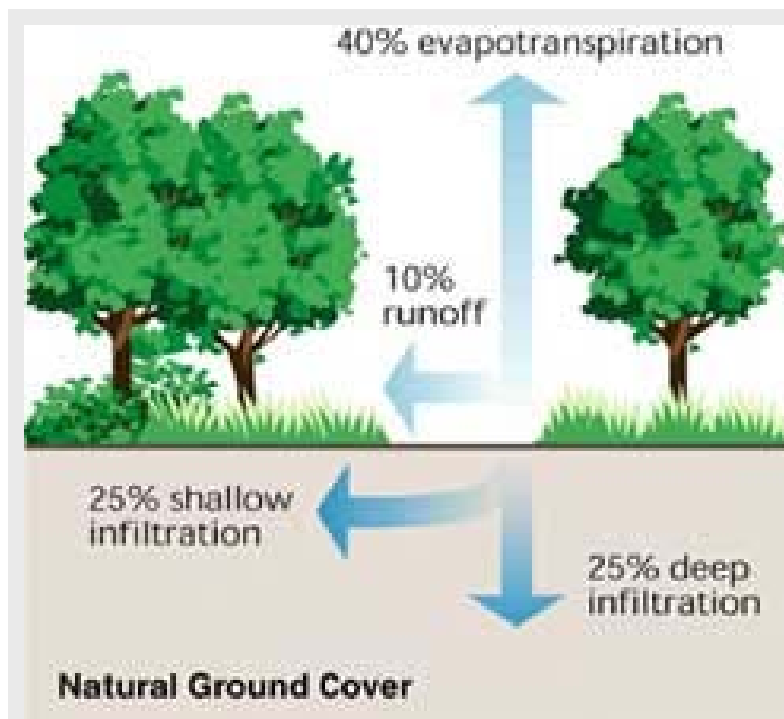
([look up in table](#))

I = rainfall intensity (mm/hr)

Rational runoff Coefficient

Description of Area	C
Business	
Downtown	0.70–0.95
Neighborhood	0.50–0.70
Residential	
Single-family	0.30–0.50
Multiunits, detached	0.40–0.60
Multiunits, attached	0.60–0.75
Residential suburban	0.25–0.40
Apartment	0.50–0.70
Industrial	
Light	0.50–0.80
Heavy	0.60–0.90
Parks, cemeteries	0.10–0.25
Playgrounds	0.20–0.35
Railroad yard	0.20–0.35
Unimproved	0.10–0.30
<i>Character of surface</i>	
Pavement	
Asphalt and concrete	0.70–0.95
Brick	0.70–0.85
Roofs	0.75–0.95
Lawns, sandy soil	
Flat, up to 2% grade	0.05–0.10
Average, 2%–7% grade	0.10–0.15
Steep, over 7%	0.15–0.20
Lawns, heavy soil	
Flat, up to 2% grade	0.13–0.17
Average, 2%–7% grade	0.18–0.22
Steep, over 7%	0.25–0.35

Source: American Society of Civil Engineers, "Design and Construction of Sanitary and Storm Sewers," *Manuals and Reports of Engineering Practice No. 37*, 1970.



$$\Delta V/\Delta t = P_n + \mathbf{S_i} + G_i - ET - \mathbf{S_o} - G_o \pm T$$

Surface flow

Streamflow

$$S_{(i \text{ or } o)} = A_x v$$

A_x = area (cross sect) (m²)

v = mean velocity (m/s)

$$v = (1/n)R^{2/3}S^{1/2}$$

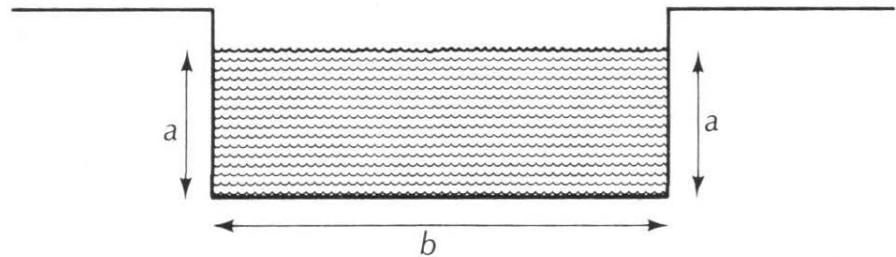
R = hydraulic radius

S = energy gradient (~ slope)

n = manning roughness coefficient

$$R = A_x/wp$$

wp = wetted perimeter (m) (don't include surface)

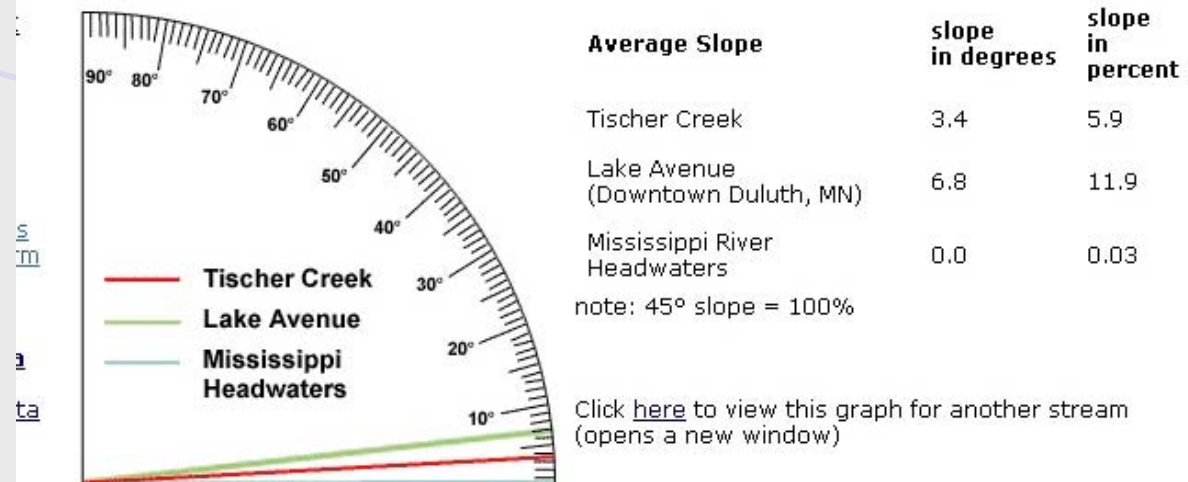


Manning's roughness coefficients

Stream Type	Manning's n
Canal or ditch	0.02
Winding natural stream , few plants	0.035
Rocky, mountain stream	0.04-0.05
Winding stream, lots of plants	0.042-0.052
Sluggish stream, lots of plants	0.065
Very sluggish stream, lots of plants	0.112

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Slope



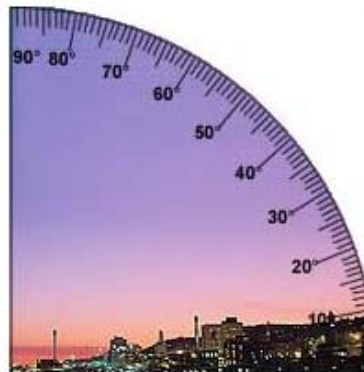
Remember that the graph represents AVERAGE slope. Some sections of the stream or road may be steeper, while other sections are less steep.

Flat as Farmland?

Lake Avenue in downtown Duluth, with a slope of 11.9% or 6.8°, is a pretty steep street - REALLY!

The lines on the graph above look pretty flat, but consider the following:

- The maximum street slope allowed by the MN Department of Transportation for new road construction is 12% or 6.8° (and only 3% or 1.7° on freeways)
- Sand dunes (that can be very difficult to climb!) have maximum slopes of 68% or 34°.



The Duluth, MN hillside at 9°



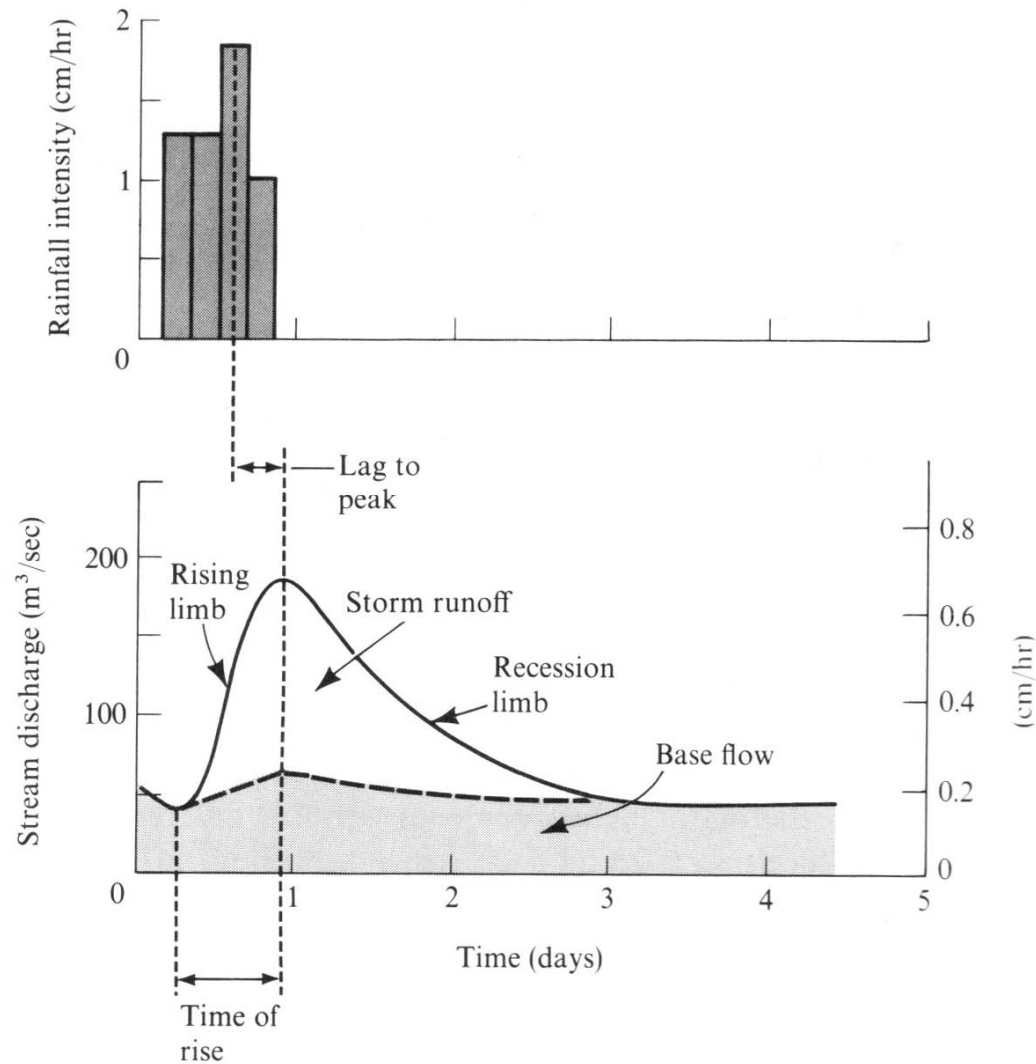
This steep sand dune is only 22°



A challenging ski slope - only 40°!

[Back](#)

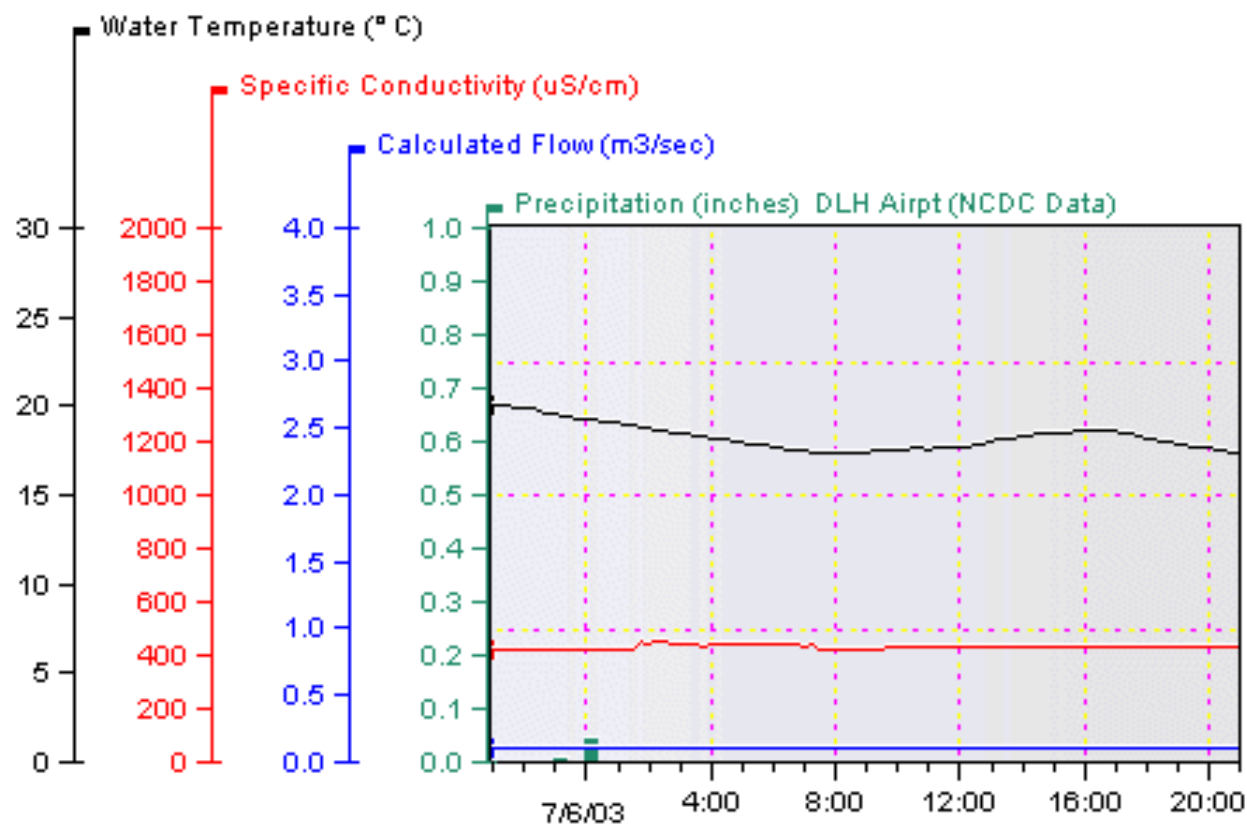
Floods and Wetlands



Dunne and
Leopold 1978

Tischer Creek, Duluth, MN

Mapping: Turbidity (NTU)

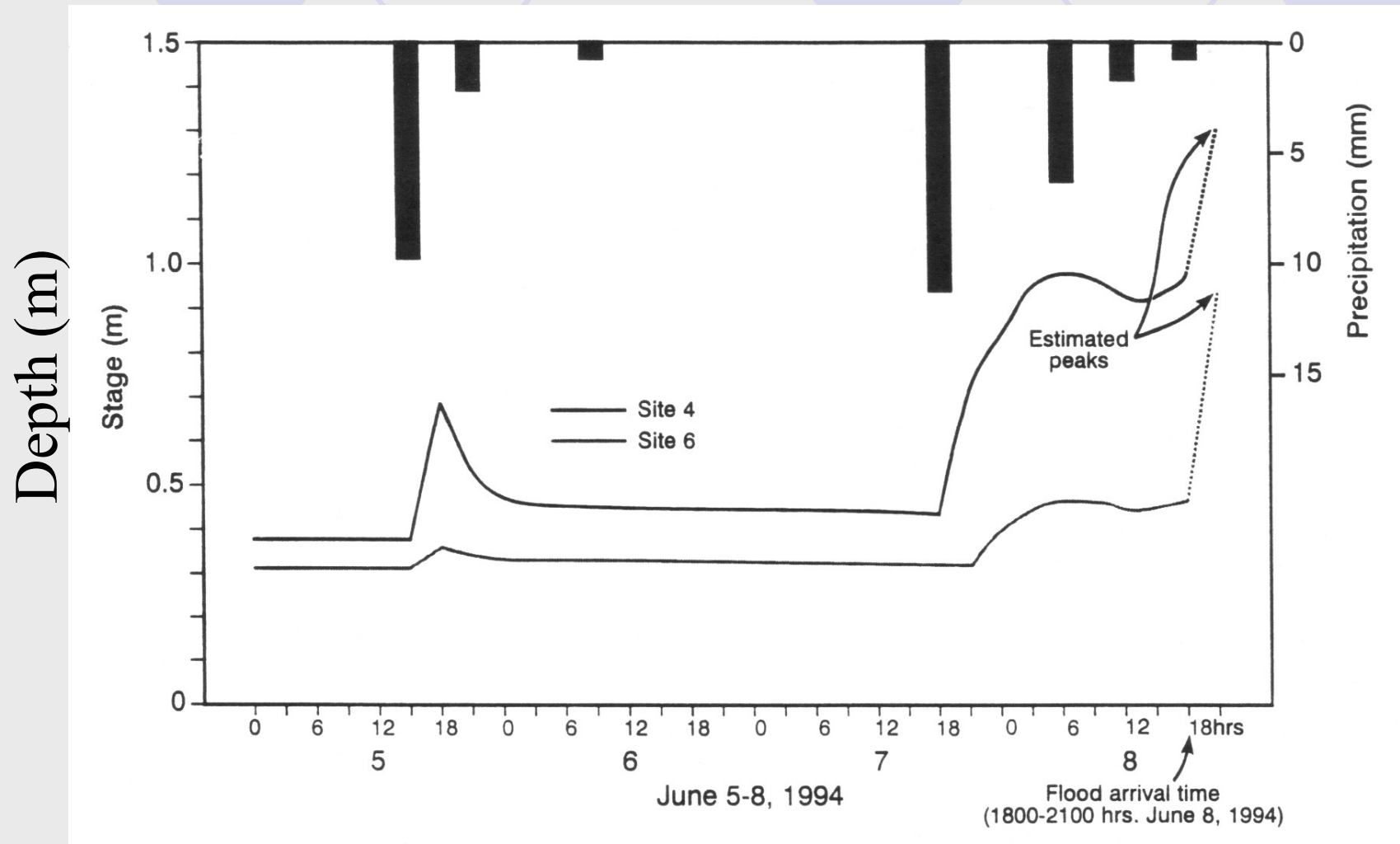


-3d.

▲ = Probe Calibration

Each bar displays data accumulated during that 1 hour period

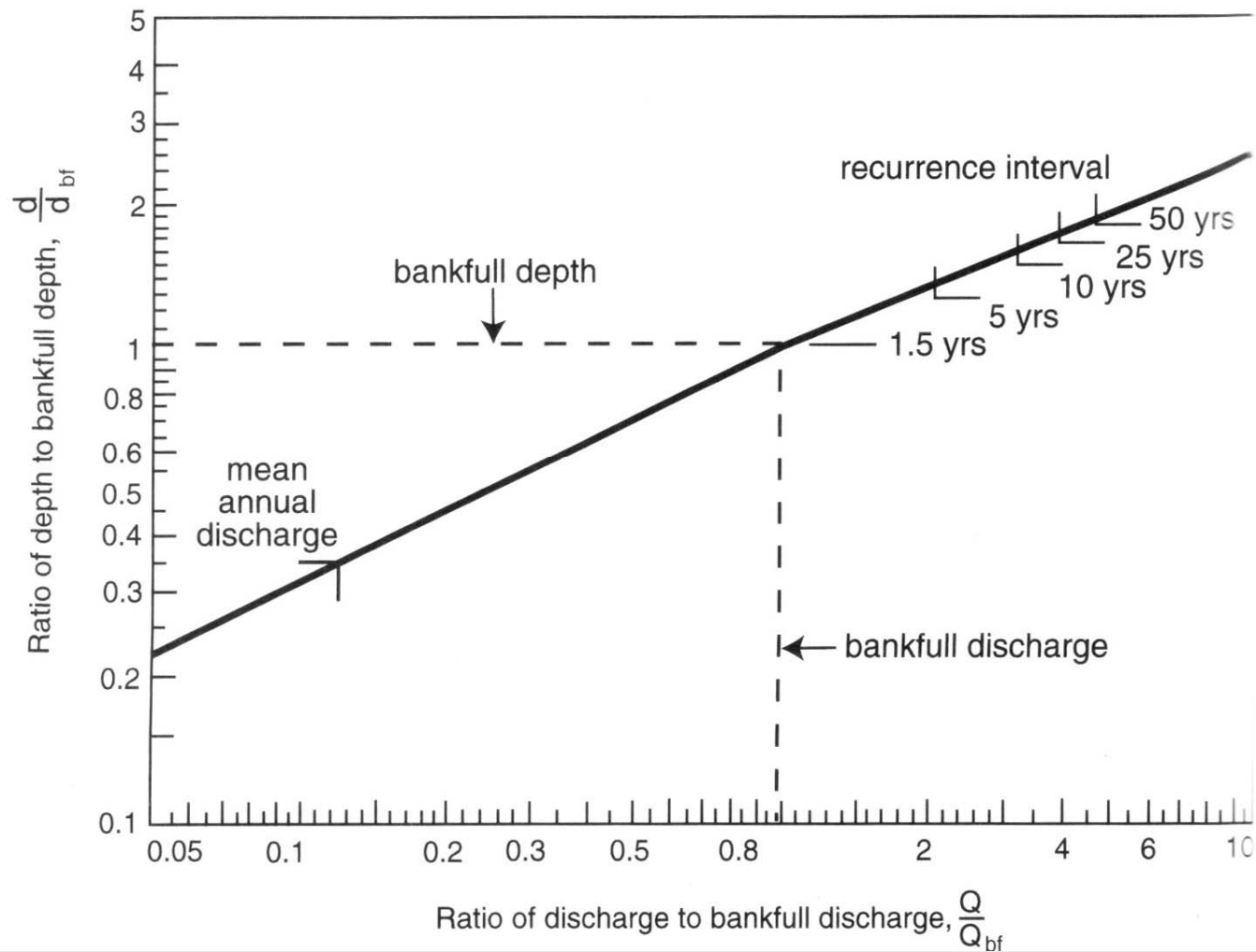
Beaver pond and wetland effects

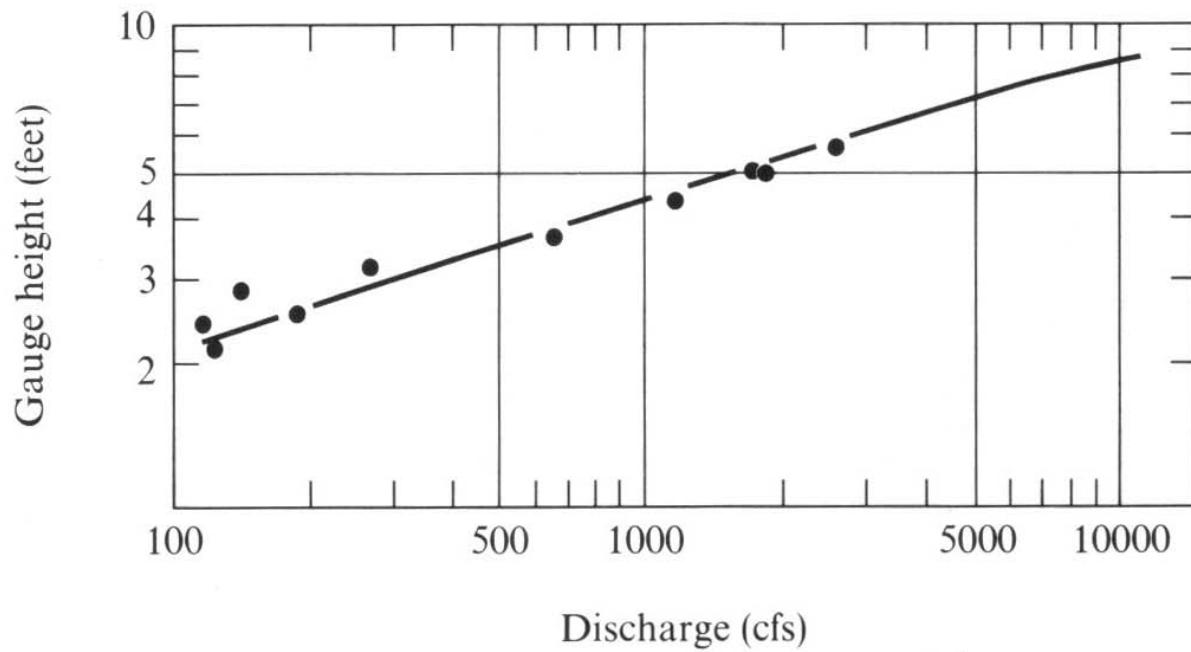


Time (hrs)

Hillman 1998 (Wetlands)

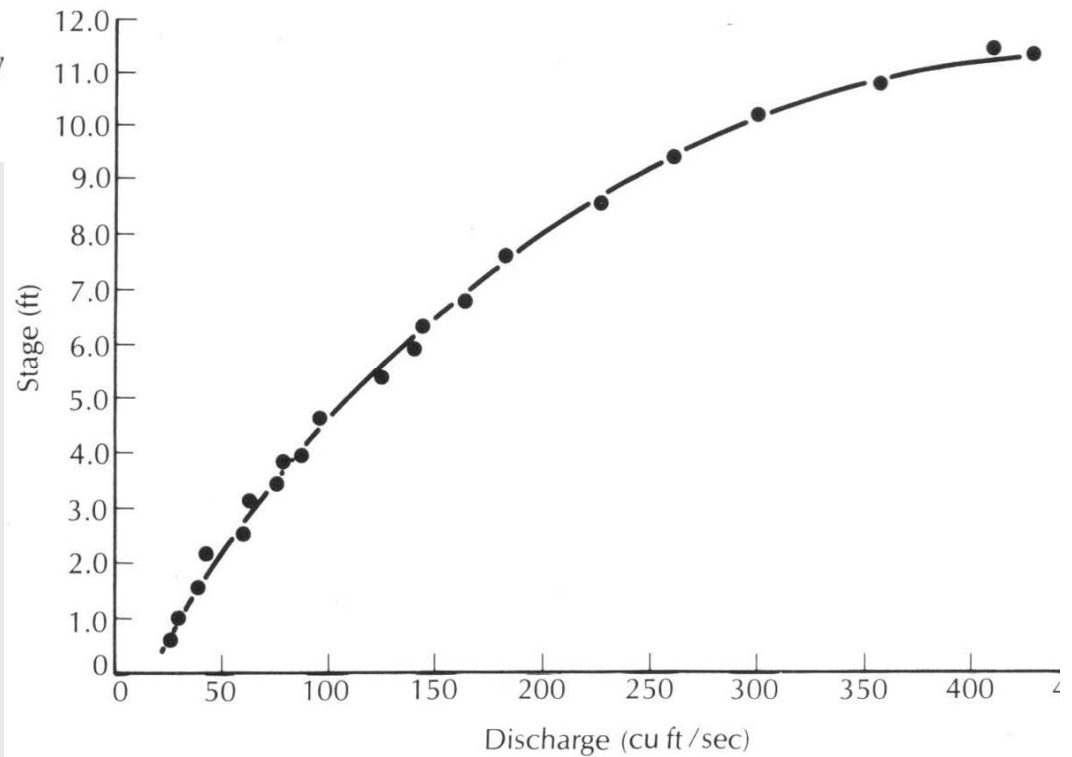
Floods and Wetlands





Rating curves

Figure 16-4 Rating curve for the New Fork Riv Wyoming.



Strahler stream order

